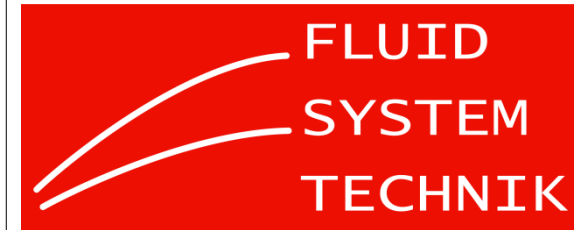


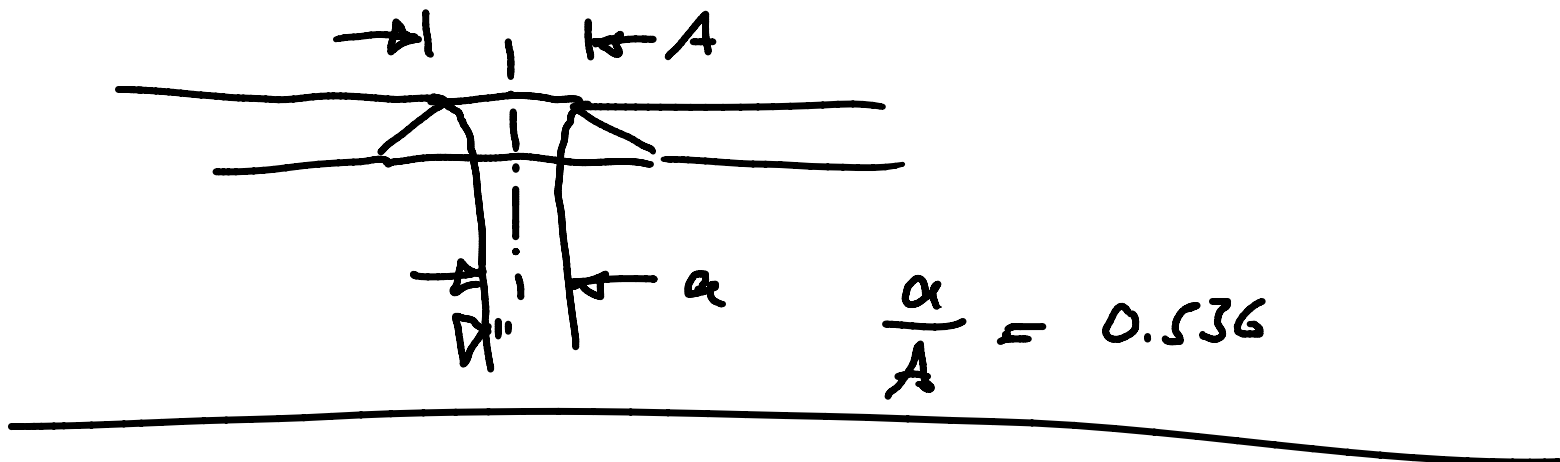
Laminare Schichten & Mischung



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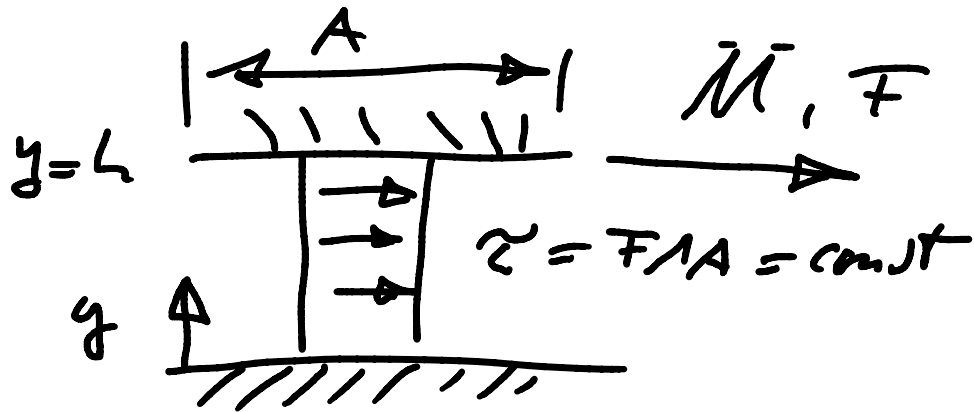


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Schichtfließströmungen



Schleppströmung
od.
Couetteströmung

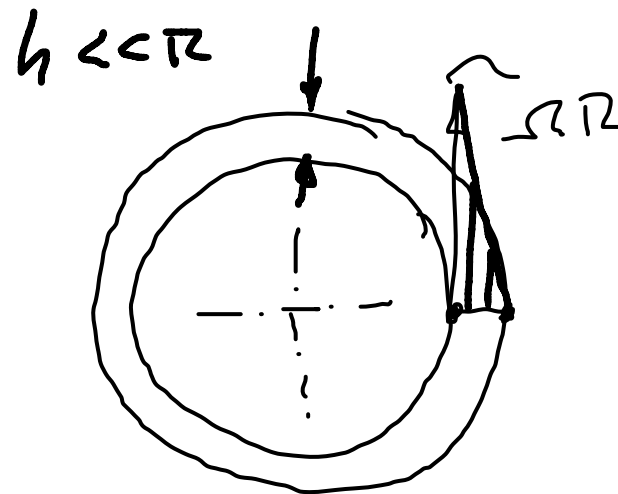
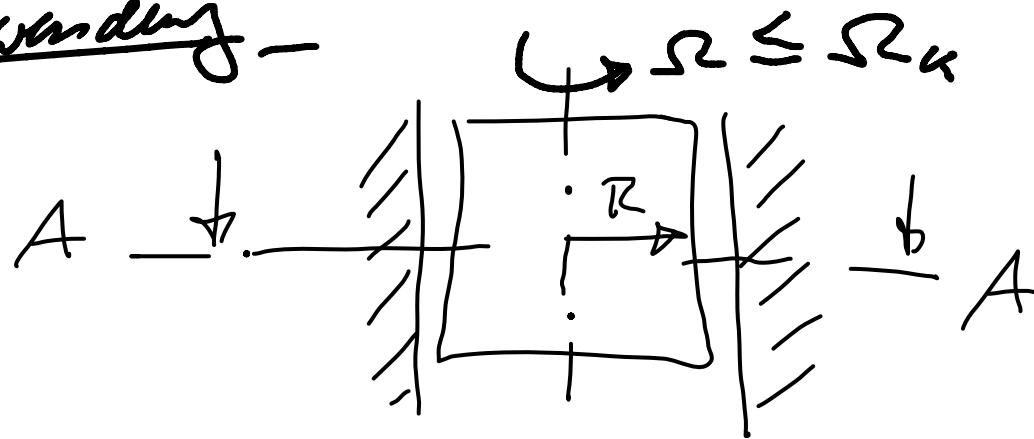
$$\tau = \eta \frac{dM}{dy}$$

$$\frac{\tau_w}{\eta} y + C_1 = u(y)$$

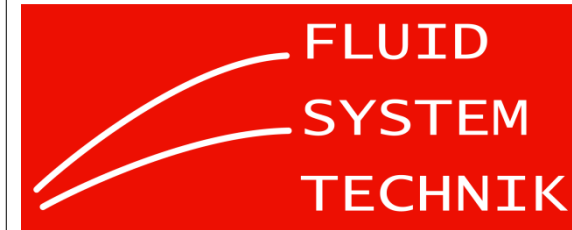
$$u(y=0) \leadsto C_1 = 0$$

$$u(y) = \frac{\tau_w}{\eta} y = \frac{\dot{M}}{h} y$$

Anwendung -



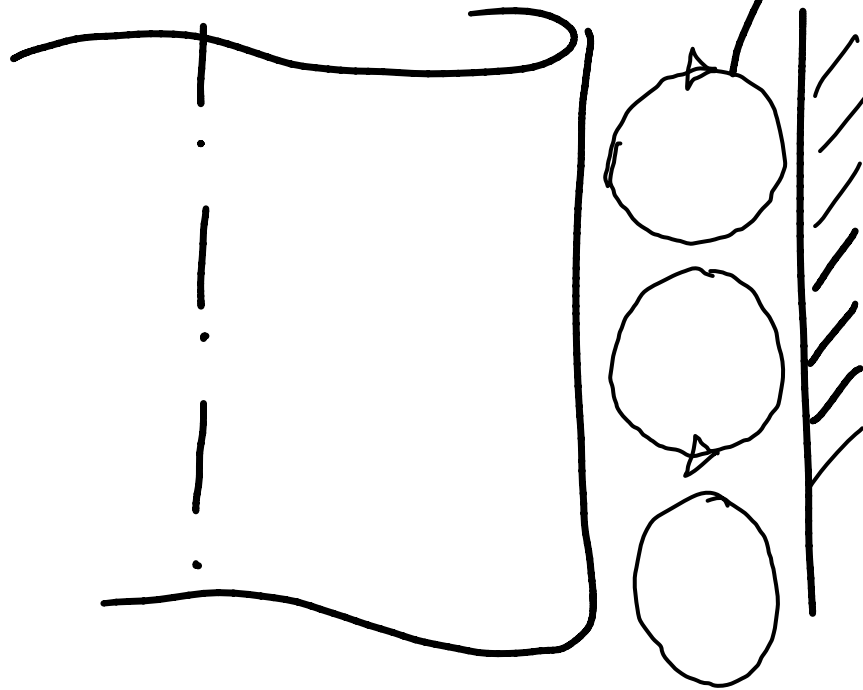
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$\Omega \approx \Omega_k$ kritische Drehzahl.

Stabilitätsproblem



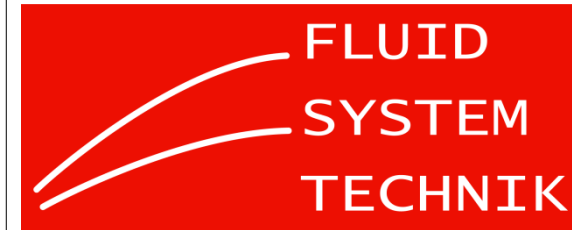
Taylor-Virbel

\leadsto keine
Schichtströmung

$\Omega \gg \Omega_k \leadsto$ Turbulenz.

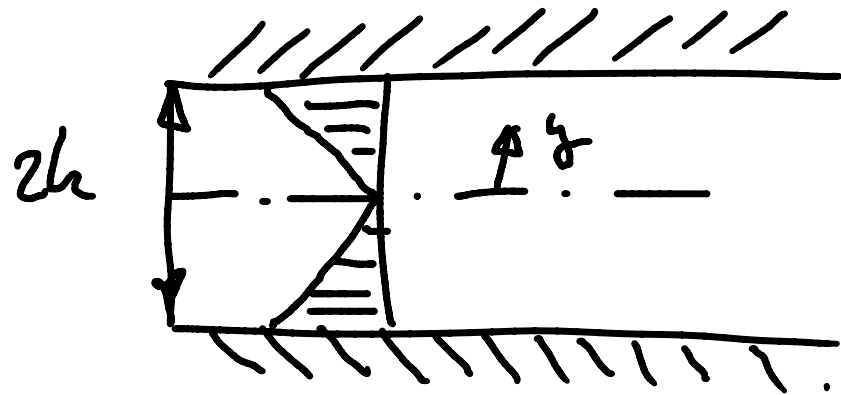


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Poiseuille-Strömung



$$\frac{\partial p}{\partial x} = \frac{d\tau}{dy}$$

$$\tau = -\tau_w \frac{y}{h}$$

$$\tau = \eta \frac{dv}{dy}$$

$$\frac{\partial p}{\partial x} = \eta \frac{\partial^2 v}{\partial y^2} \quad \text{für} \quad \frac{\partial v}{\partial t} \equiv 0$$

x-Komponente der Bewegungsgleichung
für ein Flüssigkeitsteilchen
linear Newtonsche Flüssigkeit.

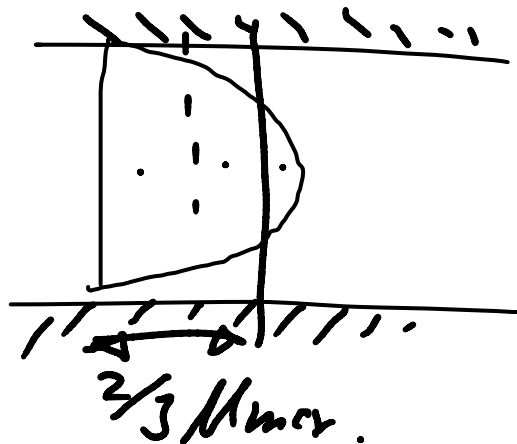


$$u(y) = \frac{K (2h)^2}{2\eta} \left(1 - \frac{y}{2h}\right) \left(\frac{y}{2h}\right).$$

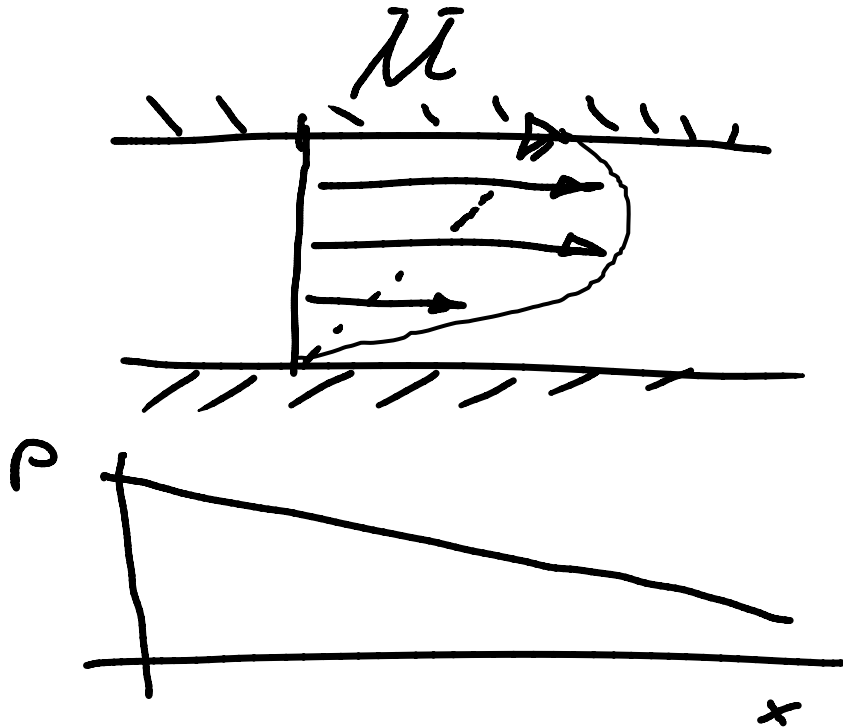
$$\bar{u} = \frac{1}{2h} \int u(y) dy = \frac{K (2h)^2}{12\eta}$$

$$K := - \frac{dP}{dx}.$$

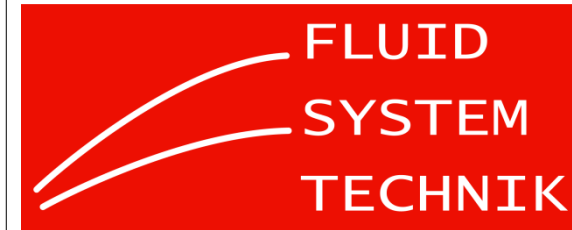
$$u_{max} = \frac{3}{2} \bar{u}$$



Überlagerung von Dreh- und Schleppströmung



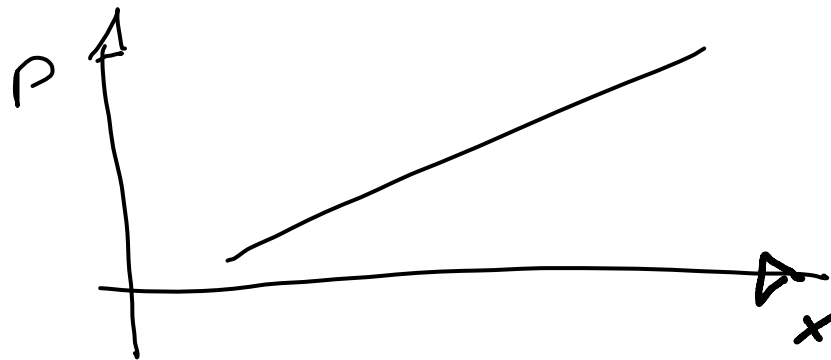
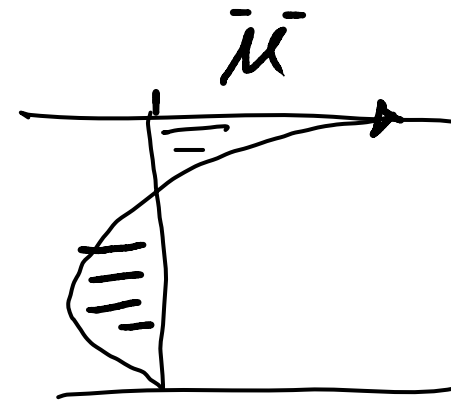
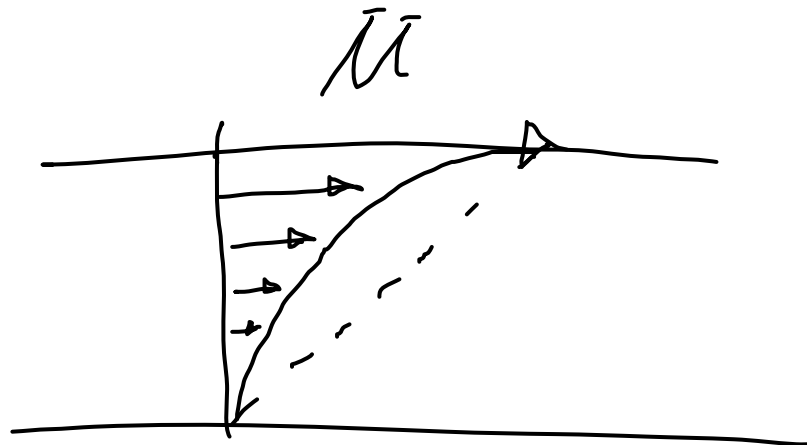
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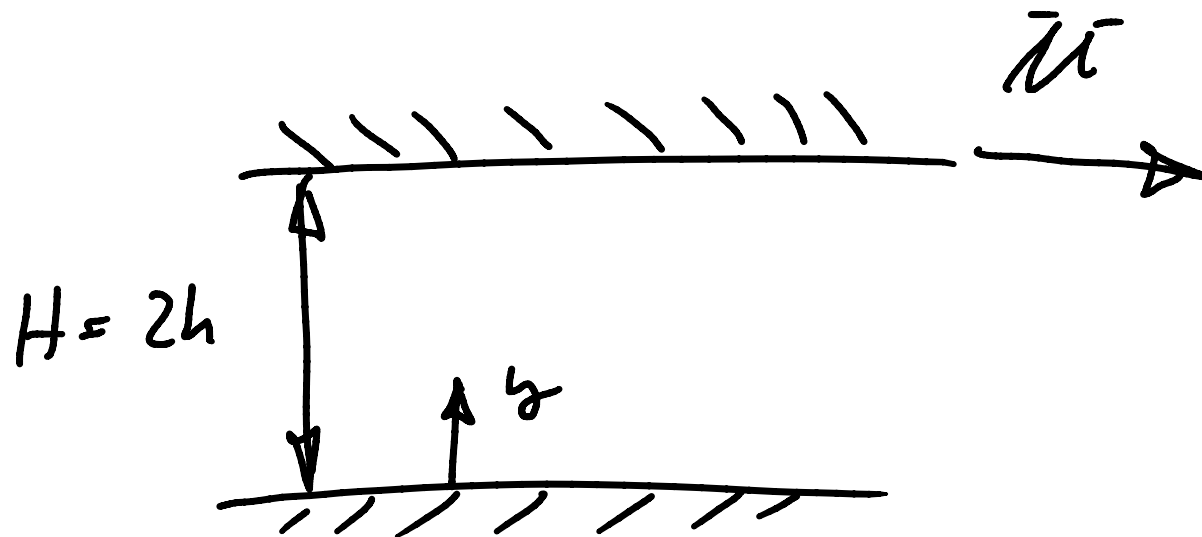


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$$\mu \quad M(y) = \frac{y}{H} \bar{M} + \frac{kH^2}{2\mu} \left(1 - \frac{y}{H}\right) \frac{y}{H}$$

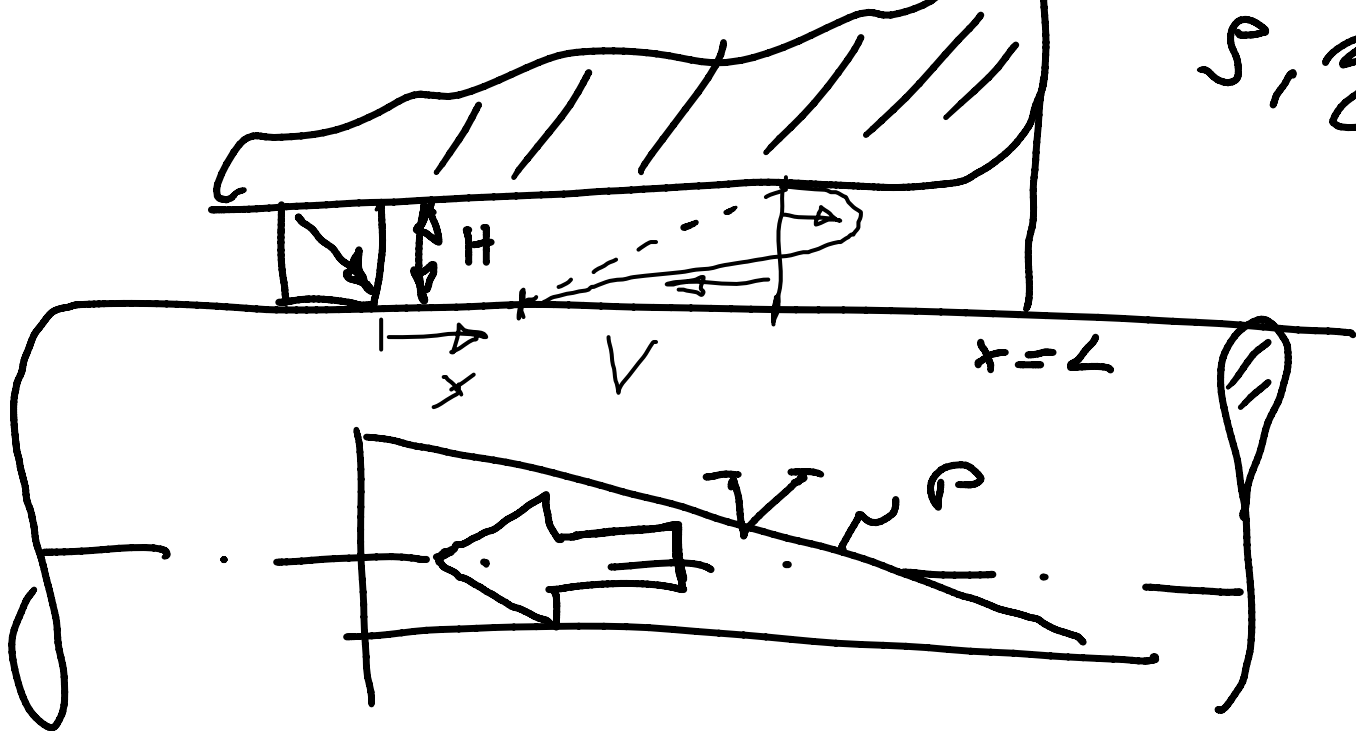


$$\bar{M} = \frac{1}{2} M + \frac{kH^2}{12\mu}$$

Anwendung Klausuraufgabe

02

S, 2



$\bar{u} \equiv 0$ im beschleunigten Fall.

$$\leadsto \kappa = - \frac{dp}{dx} = - \frac{v}{2} \dots \dots$$



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FLUID
SYSTEM
TECHNIK



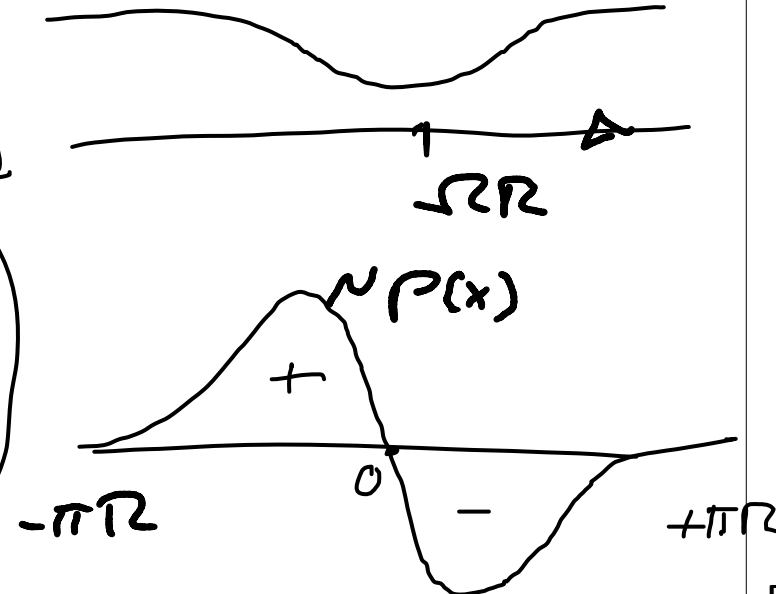
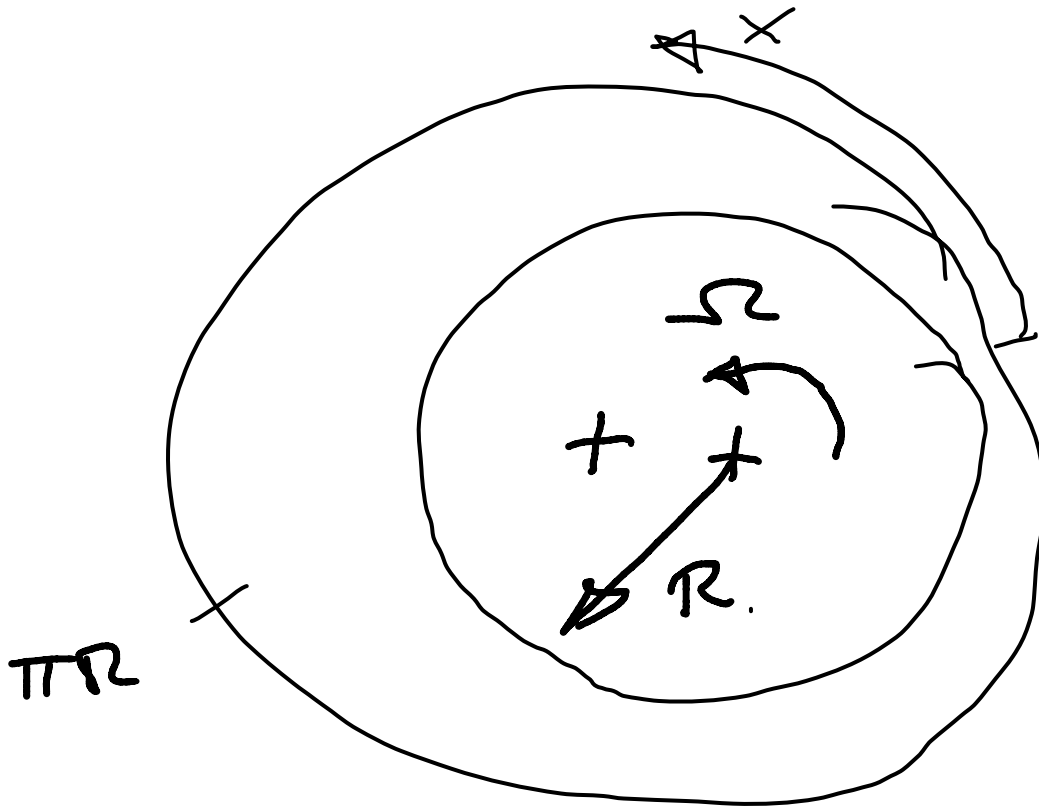
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Technisch wichtig:

Hydrodynamische Geze

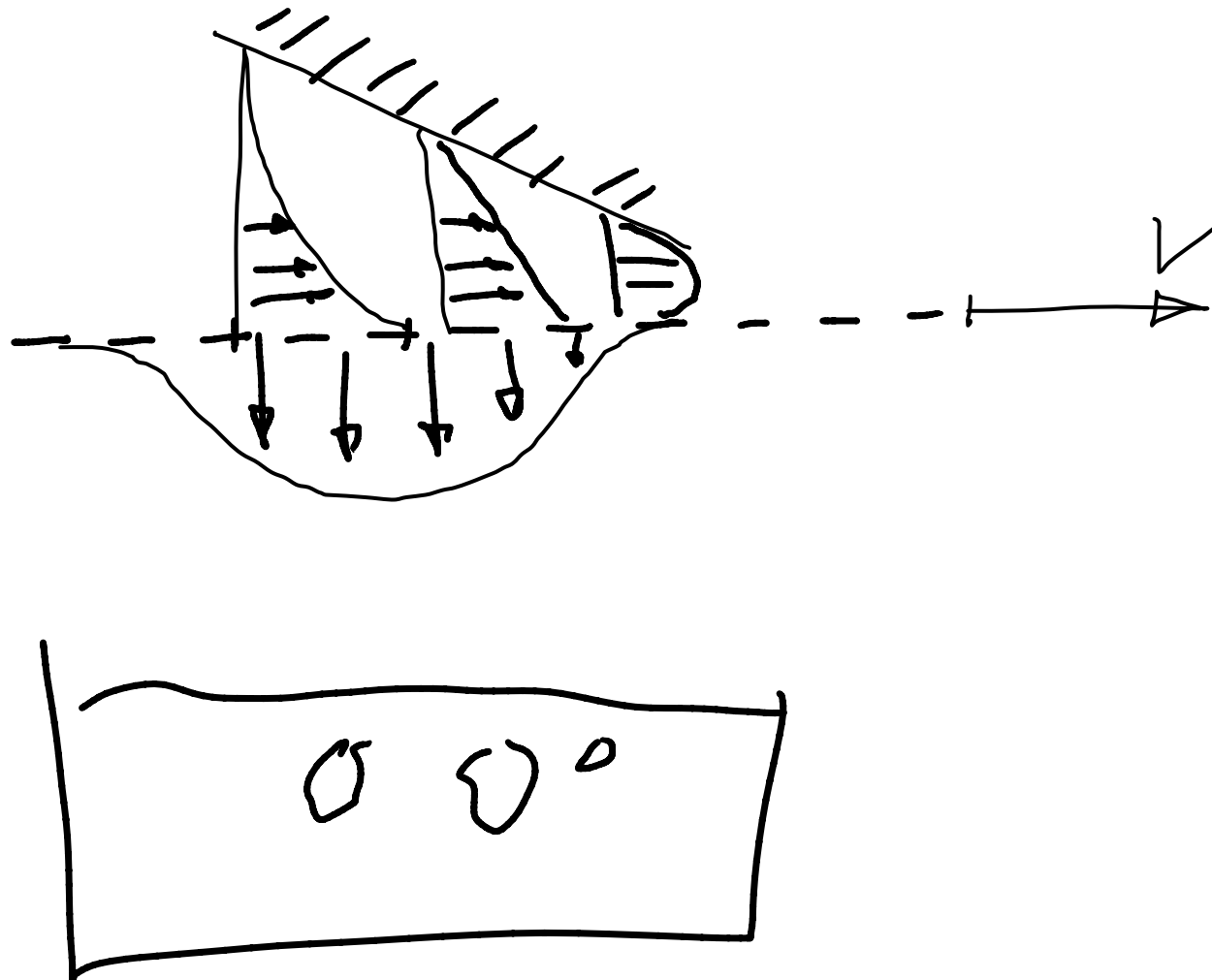
$$\alpha Re \ll 1; \alpha = \frac{dh}{dx}$$



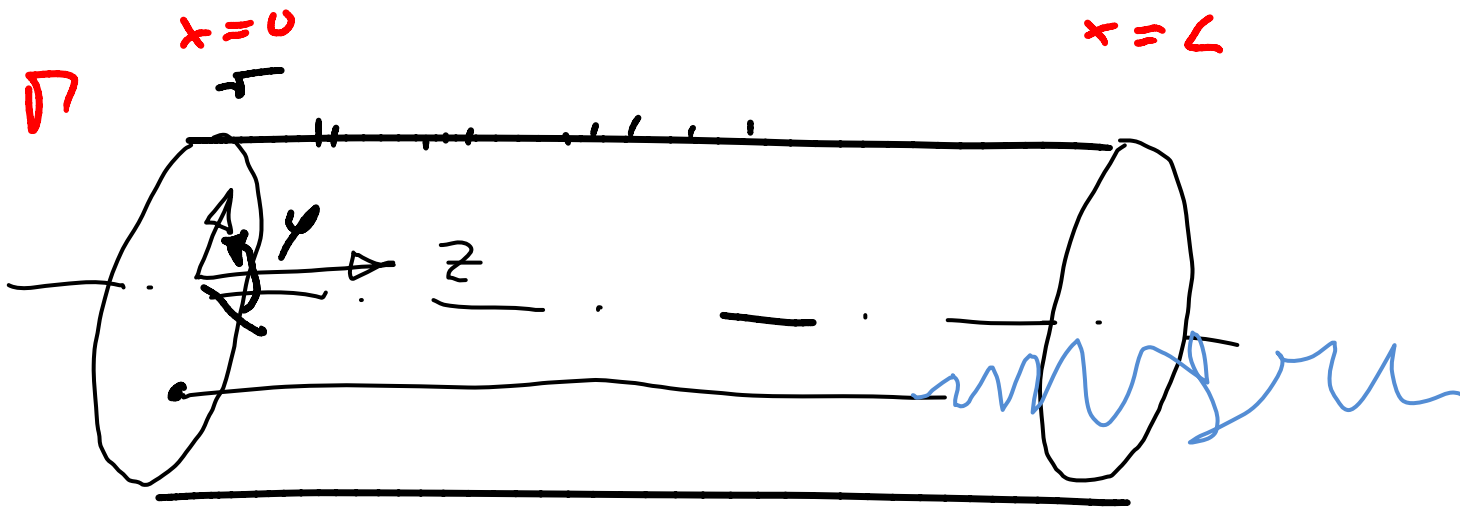
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Strömung durch ein Kreisrohr



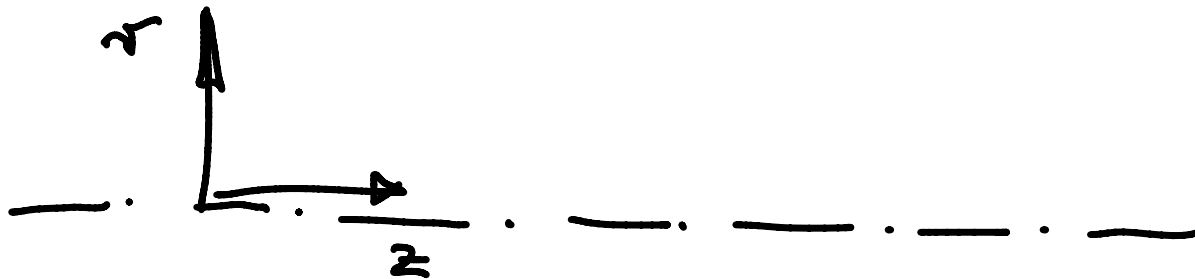
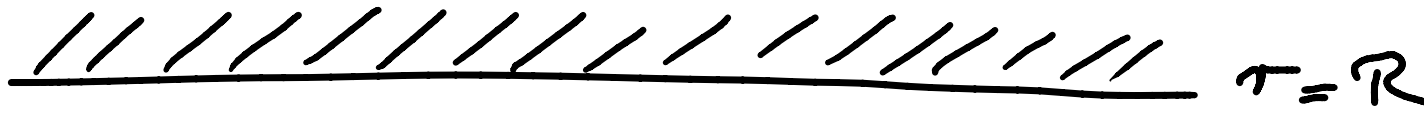
$$\vec{u} = \underbrace{u_z}_{\equiv ?} \vec{e}_z + \underbrace{u_\phi}_{\equiv 0} \vec{e}_\phi + \underbrace{u_r}_{\equiv 0} \vec{e}_r \quad \leadsto \quad u_z(r) = ?$$

für eine
drehfrei Ström.

$\equiv 0$ bei unendlich kleinen
Viskosität für die
laminare Ström.

$u_r \neq 0$ bei turbulenter
Ström.





$$\rho \frac{D\vec{u}}{Dt} = -\nabla p + \nabla \cdot \tilde{\mathcal{P}} \quad | \quad \bullet \vec{e}_z \text{ Cauchy-Schiet}$$

$$\text{für } \tilde{\mathcal{T}} = -p \tilde{\mathcal{T}} + \tilde{\mathcal{P}}$$

$$\tilde{\mathcal{P}} = \tau_{xx} \vec{e}_x \vec{e}_x + \tau_{xy} \vec{e}_x \vec{e}_y + \tau_{xz} \vec{e}_x \vec{e}_z + \\ + \tau_{yx} \vec{e}_y \vec{e}_x + \tau_{yy} \vec{e}_y \vec{e}_y + \tau_{yz} \vec{e}_y \vec{e}_z + \\ \dots$$

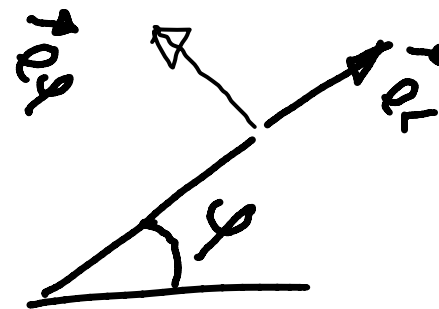


$$\rho \frac{D u_z}{D t} = - \frac{dP}{dz} + \frac{1}{r} \frac{\partial}{\partial r} (r \tau_{rz})$$

$$(\nabla \cdot \underline{P}) \cdot \vec{e}_z$$

Achtung im Krümmenlinigen Koordinaten
(Zylinderkoordinaten, Kugelkoordinaten)

$$\vec{e}_r \quad \vec{e}_\varphi \quad \vec{e}_z$$



$$\frac{\partial \vec{e}_r}{\partial \varphi} = \vec{e}_\varphi$$

no Tipp: Anfang Spalte



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$$\Delta \bar{\Phi} = \frac{\partial^2 \bar{\Phi}}{\partial z^2} + \frac{1}{r} \frac{\partial \bar{\Phi}}{\partial r} + \frac{\partial^2 \bar{\Phi}}{\partial r^2} + \frac{1}{r^2} \frac{\partial^2 \bar{\Phi}}{\partial \varphi^2}$$

Dimensionskontrolle!

$\equiv \sigma$ stationäre Schichtstr.

$$\rho \frac{\partial u_z}{\partial t} + \dots = -\frac{dp}{dz} + \frac{1}{r} \frac{d}{dr} (r_{r2} \tau)$$

$$-\frac{dp}{dz} = \bar{K} + \hat{K} e^{i\Omega t}$$

$$u_z = \bar{u}_z + \hat{u}_z e^{i\Omega t}$$

$$r_{r2} = \bar{r}_{r2} + \hat{r}_{r2} e^{i\Omega t}$$





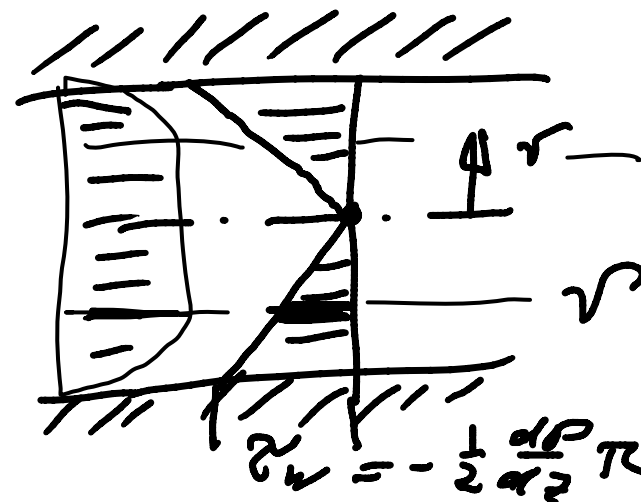
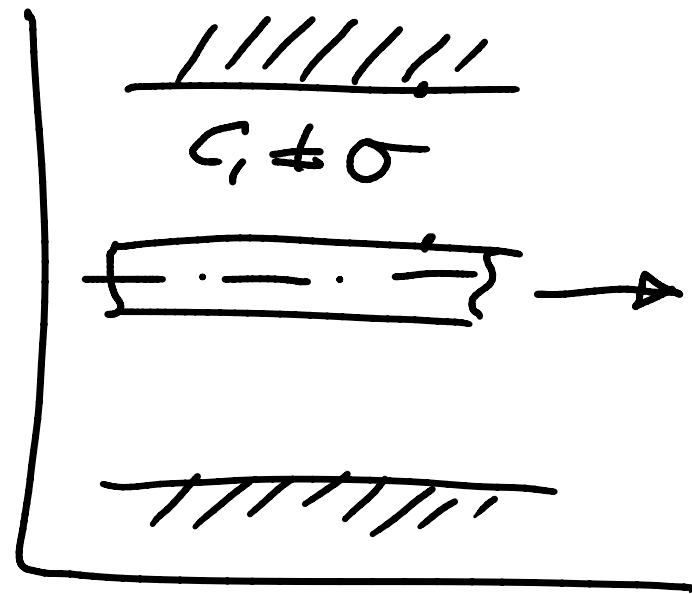
$$\frac{dP}{dz} r = \frac{d}{dr} (\tau r)$$

$$\frac{1}{2} \frac{dP}{dz} r^2 + C_1 = \tau r$$

$$\frac{1}{2} \frac{dP}{dz} r + \frac{C_1}{r} = \tau \leadsto C_1 = 0$$

$$\tau = \frac{1}{2} \frac{dP}{dz} r$$

$$\tau = -\tau_w \frac{r}{R}$$



Für die Newtonsche Flüssigkeit

$$\tau = \eta \frac{dU}{dr}$$

$$\tau = -\tau_w \frac{r}{R}$$

$$-\frac{\tau_w}{\eta} \frac{r}{R} = \frac{dU}{dr}$$

$$-\frac{\tau_w}{2\eta} \frac{r^2}{R} + C_2 = U(r)$$

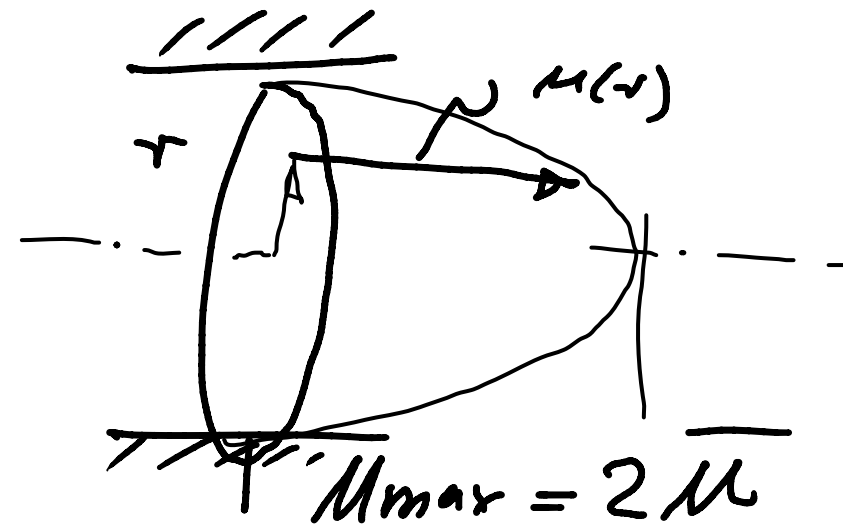
$U(r=R) \equiv 0$ Haftbedingung..

$$\leadsto C_2 = \frac{\tau_w R}{2\eta}$$





$$\mu(r) = R \frac{\tau \omega}{2\gamma} \left(1 - \left(\frac{r}{R} \right)^2 \right).$$



Rotationsparaboloid

Hagen-Poiseuille-Strömung.

Zusammenhang Volumenstrom
und Druckabfall (viskose Durchströmung)

$$\dot{V} = \int_0^R \int_0^{2\pi} u(r) r dy d\tau$$

$$= \underbrace{\frac{\kappa R^2}{8\eta}}_{\bar{u}} \underbrace{\pi R^2}_A$$

$$\bar{u} := \frac{\dot{V}}{A}$$



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$$\Delta P_v := \frac{8}{2} \bar{\mu}^2 \int$$

$$:= \frac{8}{2} \bar{\mu}^2 \left(\frac{L}{d} \lambda \right)$$

λ Durchmesser pro Längeneinheit.

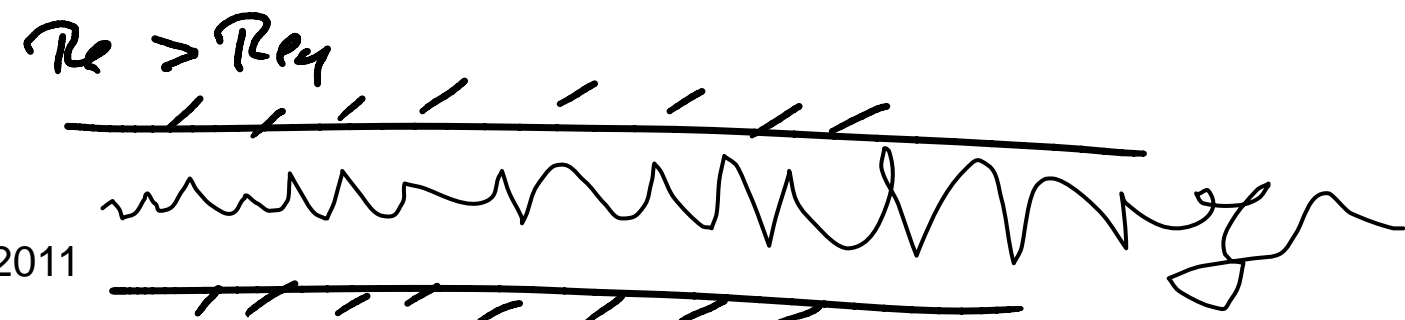
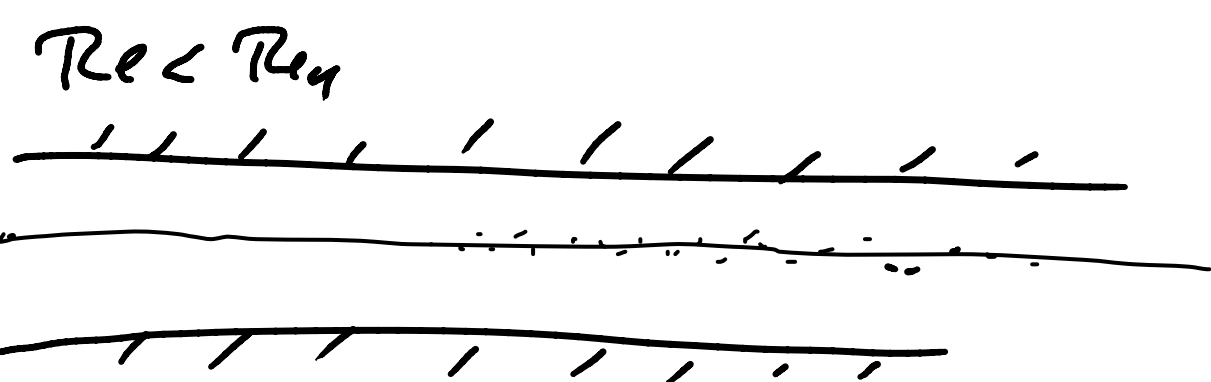
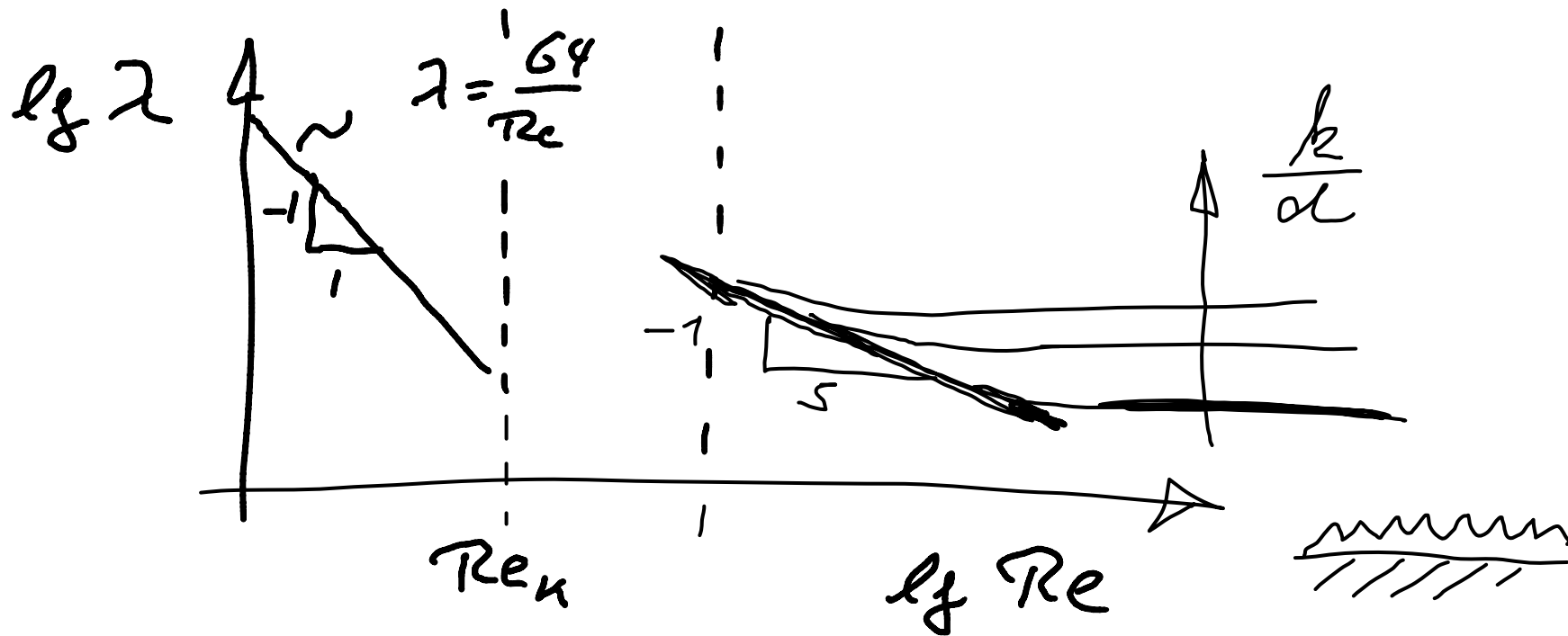
$$d = 2R.$$

$$\lambda = \frac{64}{Re}$$

$$Re = \frac{\bar{\mu} d}{\nu}$$

$$\nu = \eta / \rho$$





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